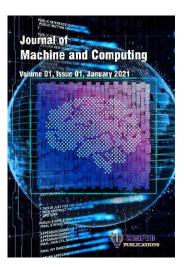
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Innovative Aerodynamic and Fault-Tolerant Control for VSVP Wind Turbines and DFIG Using Predictive and Sliding Mode Techniques

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Abstract:

To maximize power production efficiency and preserve stability under atic ci mstances, iging c renewable energy systems, especially VSVP wind turbines, must be integrated in wer grid. Wind speed he changes and grid disruptions influence their performance. This paper suggests an enh red hybrid control system for Doubly Fed Induction Generator (DFIG)--based wind turbines to optimize aero performance, power lyna collection, and fault resilience. This study aims to improve power extraction ef ency and Fault Ride-Through (FRT) capacity by merging MPC and SMC. Dynamically adjusting le and generator torque optimizes tch > power coefficient (Cp) and reduces pitch angle variation, rotor spee luati ns, and reaction time. For fault mitigation during voltage dips, Higher-Order Sliding Mode Control (H d the Super-Twisting Algorithm (MC) (STA) modulate DFIG electromagnetic force to require ples, mugate the voltage sags, and minimize THD. MATLAB implements the framework. In roved fficient (Cp) of 0.52 at $\lambda = 6.5$ surpasses PI wer d 1.8%, 9 (0.42) and Fuzzy Logic (0.48) controllers. THD pared to 5.5% (PI) and 2.3% (Fuzzy Logic), assuring improved power quality. Torque ripple is reduce 2.1%, stabilizing turbines. The suggested technique increases FRT, energy capture, and grid stability. Or dual-layer control approach may improve wind turbine efficiency, dependability, and resilience under changeable rind and grid circumstances.

Keywords: Predictive Control, Slight Control, Variable Speed Variable Pitch Wind Turbines, DFIG, Voltage Dips

1. Introduction

Due to their need for lawless lectrical network integration, wind turbines have emerged as crucial components of ten rarv newable energy systems [1]. Wind turbines with VSS/VSP designs operating aspects to fit varied wind conditions, maximizing their power automatic modi city [2] Active modifications to blade pitch and rotor speed are made possible by the gener VSVP wind turbines, allowing them to enhance power efficiency [3]. Maximum control ems used component strain are both made feasible by wind turbines' adaptable functioning outp ral operational challenges prevent the addition of variable renewable power sources, 41. wind energy output, to the current electrical power infrastructure [5]. Power variations icular variable wind energy production undermine power grid stability and quality requirements caus Rapid changes in wind speed may cause voltage variations at the electrical supply level, which can affect electricity dependability [7]. Power electronic converters and intricate control systems allow modern wind turbines to operate at varied speeds while still being friendly to the grid [8]. Turbines are able to operate at their maximum efficiency with the help of power electronic converters, which isolate the generators from the grid and allow them to manage reactive power and low voltage immunity [9].

Intelligent scheduling and operational control systems are necessary for the proper integration of wind energy into the power grid [10]. When wind farms connect to the grid, the development process generates grid codes that the power plants must follow in order to operate reliably and steadily. When electrical network problems occur, modern wind turbines include sophisticated features that provide necessary ancillary services to maintain voltage support and frequency balance [11], [12]. Supply stability issues caused by uncertain power availability may be addressed with the use of smart grid technology, energy storage, and improved forecasting tools for older power systems. The increasing usage of wind energy makes it all the more important to study how to make wind turbines more efficient and how to make power grids more stable. An in-depth familiarity with wind turbine performance, grid power distribution, and environmental factors is necessary for research into the development of provide and dependable systems [13]. By addressing these problems, wind energy can continue to play a crue l role in creating a renewable energy power infrastructure that can withstand the test of time.

1.1 Problem Statement

Unpredictable wind changes and grid failures make VSVP wind turbine *instable* miting eir power ator torque. Because extraction capabilities, which is controlled by adjusting the pitch angle an ep voltage dips generate torque oscillations and electromagnetic disturbances, which reduce power quality, they have a detrimental impact on DFIG-based wind turbines [14]. Pow trol techniques are ful & required to enhance system power performance and fault preventi pathities, since the Proportional-Integral (PI) controllers are unable to handle nonlinear process disturbances. s an

1.2 Existing Solutions & Limitations

QFIG systems, a number of conventional In order to control VSVP wind turbines in co nch ol has een widely used because to its usermethods are used. While Proportional-In gral co ities and grid events. Since Fuzzy Logic Control friendliness, it falls short when faced with no (FLC) systems respond well to uncertainty, the edictability of dynamic wind conditions is reduced when utilizing them [15]. Although Adaptive Catrol may operate in real-time, its significant computational complexity makes it application for such applications [16]. Chattering is an undesirable side effect that has a detrimental system performance caused by Sliding Mode Control's heet the present demands of control strategy, DFIG-based resilience against nonlinearitie (In order to wind turbine applications need better approach that optimizes aerodynamic outcomes and reliably ilithe during voltage drop situations. offers fault ride-through cap

1.3 Research Motiv tion

This stud duar-control strategy for DFIG-based wind turbines that improves power sent mainta s grid stability during faults by integrating Model Predictive Control with produ haracteristics of Super-Twisting Algorithm and Higher-Order SMC. By using real-Advan SMC torque control based on MPC, the proposed technique seeks to maximize aerodynamic time tch a By using STA-SMC for smooth control activities and HOSMC for torque oscillation efficien uction the system is able to achieve better FRT capacity. In the event of a power outage, put a in in place to reduce electromagnetic interference and improve the quality of the electric mee **g**r. The framework integrates several control strategies to maximize electricity production while ensuring grid stability.

1.4 Research Significance

Optimizing operational performance of DFIG-based wind turbines in the face of grid interruption events and variations in wind speed is the focus of this study. The designed framework optimizes the pitch angle and generator torque in real-time to achieve optimal efficiency in energy collecting. This system design enhances power system stability, complies with grid rules, and keeps turbines stable even when voltage decreases. To improve operating efficiency and equipment lifespan length, the presented technology works to lessen torque variations and Total Harmonic Distortion. When renewable energy systems use the suggested approach to power quality and grid integration, they become more resistant to electrical disturbances. More efficient and fault-tolerant modern wind power generating systems are the result of actively resolving the main difficulties plaguing wind energy systems.

This structure is followed by the paper: In Section 1, the research challenge, including its motivation relevance, and major contributions, is explained. Current control mechanisms and their limitations reviewed in Section 2. The control framework and system modeling are presented in Section 3. Section 5 presents the outcome of the study, along with comparisons and remarks. Proposed future research directions and important findings round out the section.

2. Related Works

An automated phase angle adjustment elimination system is created by hen et d used in [17] three-turbine Savonius wind clusters to increase power output. The system le-speed controlled. var Rotational direction, configuration angles (θ 1-2, θ 1-3), and inter-turbine dist es (L1-2, L1-3) are the three main elements that are examined in the optimization process using Taguchi technique. Independently functioning wind ratios of 1.13, 1.14, and 1.09 result in a average power coefficient increase of 1.425, according to the study. Because it is sensitiv ges in wind speed and direction to cb and has difficulty scaling up efficiently as cluster sizes inc em's implementation has two ea major flaws.

Gupta et al. [18] study H-rotor Darrieus V Win Turbines (VAWT) at low wind speeds Ical Ax 2D D model mimics changing blade pitching using using dynamic blade pitching. A high-fide al effects. The NACA0015 airfoils' variable angle sliding mesh and remising to capture rotor rota of attack changes at 1.5 tip speed ratio (TSR) e anced power coefficient (Cp) by 81% to 0.44. Lengthening and adding blades im ves performance. Complex aerodynamic effects between components and mechanical lin implementation must be solved by active pitching ts d mechanisms.

Shan et al. [19] introduced Para Compact Firefly Algorithm (PCFA), which enhances performance by reducing memory ent. The compact approach works for tiny turbines and decreases equire memory needs, where the par llel technique optimizes solutions and solves quicker. PCFA tested 28 setting variable pitch wind turbine proportional-integral-derivative benchma fr umes less memory, produces better solutions, and solves problems quicker than CFA co parameters tion methods. The wind turbine control system efficiently controls output power. The compa ptim cipal initations include parameter adjustment susceptibility and computing challenges in system's p g situations. uncer 1 ope

Les adaptive fractional-order non-singular fast terminal sliding mode controller for individual pitch control of wind turbines against uncertainties and external disturbances is AFO-NFTSMC, which is a bibed in a paper by Aghaeinezhad et al., [20]. The controller is based on a two-mass model of the wind turbine and uses two subsystems to describe the mechanical and aerodynamic components, as well as connected movement equations. employing step and turbulent wind testing, the study examines controllers employing the single-blade approach. In order to verify the system, the FAST software and the TurbSim simulation tool were used. When compared to traditional adaptive and sliding mode controllers, the suggested controller showcases better rotor speed tracking capabilities and offers high accuracy performance with improved stability. There are two problems with the controller: first, it could need a lot of processing power, and second, it becomes hard to utilize in real time when the wind is very variable.

In their investigation, LeBlanc et al. [21] looked at the effects of blade pitch adjustments on the aerodynamic and structural stresses of a Vertical Axis Wind Turbine (VAWT). In the open jet wind tunnel at TU Delft, strain gauges detect the normal loading on the blades via the stressed struts while the blades are tested at various fixed pitch offsets from a neutral position. The experimental findings show that turbines are very sensitive to changes in pitch angle, leading to the occurrence of uniqu aerodynamic phenomena such as blade dynamic stall and vortex interaction. Rotor thrust characteristics and stresses acting on the rotor and platform acceleration frequencies may be controlled by adjustit the pitch, which also increases the reaction per revolution. The scalability of real-life data is affected by experimental limits and measurement error limitations in this investigation.

A fault-tolerant finite-time constant non-singular terminal synergetic control. make largescale wind turbines more dependable following simultaneous pitch ag ator fa ording to ures, t under high-wind Palanimuthu's study [22]. under addition to dependable power m gem conditions, the control system improves the accuracy of precision tracking ocedures. The control system's resistance to time-dependent disturbances and tracking capabilities a both improved by a theory is used to establish disturbance observer that uses mismatched control components. Lyapur stability and finite-time convergence. The results of the simula owing the performance of wind ions) turbines based on PMSG that are 4.8 MW and 20 MW show th y ar very reliable both before and after disturbances happen. Inconsistent modeling result real. d Joyment challenges, and very disruptive operating events make optimization control difficult. 'ste

oped self-adapting active fault-tolerant MPPT control In wind power systems, Chen et al. [23] de approach to safeguard maximum power point the ang capabilities from generator-side faults. Observer arities, and unknown disturbances like failing components estimate model uncertainties, nonly generators and disturbance torque impal time. Adjusting for estimated disturbances, an adaptive feedback linearizing control system regul s the variable-speed wind turbine (VSWT). It performs ent whole systems or measure all states or faults. Three better than typical ways since repr doe controllers outperform PI with ISSF-N controllers in adaptability, stability, and tracking error. In addition to system-re tions, the suggested technique requires external operational va confirmation testing.

tive switched sliding mode controller to improve floating wind turbine Song et a [24]performan nder a ator failures and environmental uncertainty. A switching linear model with ne characteristics simulates the system, while full-order state observers and adaptive averag vell error disturbances, and faults. The work generates control parameters using average rules han matrix inequality, and Lyapunov stability theory. FAST simulations show that the dwel ne, l ontroller runs on the NREL 5MW wind turbine with a spar-buoy platform, resulting in better ggeste ity and lower mechanical stresses than gain-scheduling PI control. Offshore facility testing and high computational needs are the key obstacles.

In order to enhance the fault tolerance of wind turbines, Fayazi et al.[25] proposed an L1 adaptivesliding mode control (L1 adaptive-SMC) system that would deal with issues such oil air content, hydraulic leakage, and pump wear. The L1 adaptive control precisely controls the rotor speed and power with sliding mode control, adjustable gain, and an integrated sliding surface. Researchers used FAST simulations to verify on a 5MW wind turbine operating at high wind speeds. Compared to

adaptive-SMC and adaptive control, L1 adaptive-SMC improves system reliability in the face of disruptions, faults, and wild wind conditions.

In order to monitor the states of the active pitch system in wind turbines when faced with unknown uncertainties, Rodríguez et al. [26] created a Fault Detection and Diagnosis approach that relies on the Takagi-Sugeno Unknown Input Observer (TS-UIO). The method allows for the identification and diagnosis of sensor faults by comparing the residuals of a TS-UIO with the system model. The approach converges to a zero estimate error by linking unknown inputs to Linear Matrix Inequalities. Effective disturbance and noise performance was shown in the simulation experiments conducted utilized reference wind turbine models. The computational complexity and the need for field experiments evaluate the system's efficiency across varied environmental conditions are the key restrictions.

To better regulate active and reactive power in doubly fed induction generators, Aoun at field-oriented control approaches to improve the energy quality of vari ind turbines. Experiments were conducted in MATLAB/Simulink that contrasted neur logic, and netwo proportional-integral controllers. Standard criteria were used to calibrate the P controller, although reducing it needed a lot of math. Despite the FLC's improved performan there was no proof of mathematical stability. A Neural Network Controller outperformed its riva in terms of tracking accuracy and dynamic response time. Training neural network control and validating wind farms in real time are both demanding tasks.

Wang et al.[28] used mechanical-electrical-grid modeling y fed induction generator grid stability and electrical damping under varied y and control settings. Machine dynamics, eet electrical behavior, and grid interactions are ed. Key findings: (1) Wind speed and mulati -vali control strategy affect shaft oscillations, a de impedance varies with wind speed; (2) For rotor constant wind speeds, control parameters affe rive train dynamics, and proportional gains in the grid integration DFIG stability insights. control system affect rotor-side impedance, offer This model is limited by its assumptions are need for real-world testing under changing grid conditions.

3. System Modeling

Figure 1 depicts the proposed and energy onversion system that makes use of V.S.V.P. wind turbines and a Doubly Fed Induction Operator, both of which function under an advanced hybrid control framework.

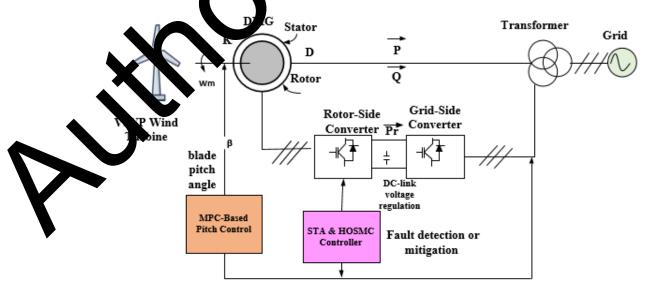


Fig. 1. Proposed Framework

The model of the wind turbine incorporates the fundamental processes involved in harnessing aerodynamic resources for power generation. The capacity to convert energy is controlled by two essential components of power coefficient efficiency. In order for the DFIG model to function, the synchronous reference frame is used as the rotational basis in two voltage equations. The rotor-side and grid-side converter systems are essential for active and reactive power transmission. The stator part receives electricity directly from the grid, while the rotor section manages the transmission of power via a back-to-back converter. Combining Sliding Mode Control with a Super-Twisting Algorithm and Higher-Order SMC for fault tolerance, this work incorporates Model Predictive Control to improve aerodynamics concurrently. While STA-SMC protects the grid from disruptions by stabilizing the voltage, the MPC real-time system regulates the pitch angle and generator torque. Optimized of track power production, increased operational stability, and a stronger link to the power grid are at outcon s of the unified modeling approach.

3.1 MPC-Based Aerodynamic Control for Power Optimization

By optimizing the power coefficient parameters with pitch angle a d tip-sp ed ratio rules, the optimization process in VSVP wind turbines using Model Predict ntrol accomplishes power extraction. To maximize efficiency in power conversion, the convolution will adaptively change the pitch angle and generator torque based on the wind condition The objective of MPC is to minimize (C_p) by making real-time adjustmenter to the pitch angle and generator torque, respectively. As shown in Equation (1), the MPC ost f Action is defined. At time step k, with a limited prediction horizon, MPC solves an op oblem. One way to express in on p the typical MPC cost function is as follows:

$$J = \sum_{k=0}^{N_p} (w_1(P_{ref} - P_{w_1} + w_2(\beta - \beta_{k-1})^2 + w_3(\tau_g, k - \tau_g, k - 1)^2)$$
(1)

J, N_pPrediction horizon, w_1, w_2, and w_3 w hting factors are the cost function to be minimized. Pitch angles at the current and previous time steps represented by β_k and $\beta_{(k-1)}$, whereas P_ref power output, respectively. Generator torque at current and and P_w stand for reference and ac e variations in roll-axial torque and glide-pitch. Control previous time steps, τ g,k- τ g,k-1 to re it in the optimized sequence is applied. In situations with Action Execution is when the f Latol in tċ partial load, the pitch mechan n modifier he blades to maximize C p while reducing g power. At the next time step, the optimization oblem is re-solved using new measurements. Maintaining Pitch and Modifying Torque A del for pitch control is: еň

$$\beta = \frac{1}{T_p} (\beta - \beta^*) \tag{2}$$

In Eqn. (7) T_p , the pitch actuator time constant. Generator Torque Control is denoted in Eqn. (3). The generator rque reference is adjusted to match the optimal torque-speed curve:

is the litch actuator time constant in Eq.(2). The symbol for Generator Torque Control is found in (3). The ideal torque-speed curve is matched by adjusting the generator torque reference:

$$r_g = k_{opt} \omega_r^2 \tag{3}$$

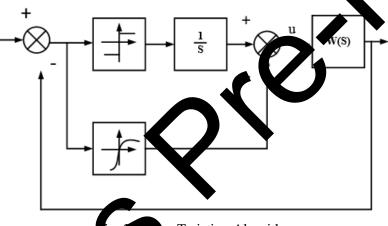
Properties of the turbine define the empirical constant k_{opt} . Details about the system's control inputs, anticipated future actions, and optimal configuration settings Pitch responsiveness, overshoot, powering efficiency, and mechanical wear Grid integration and wind response prediction analytics.

3.2 Sliding Mode Control Techniques for Fault-Tolerant DFIG Control

Enabling fault ride-through capability in the DFIG system is the primary objective of Sliding Mode Control. This feature ensures stability and efficacy in the face of grid voltage dips and disturbances. Torque oscillations, significant total harmonic distortion (THD), and voltage instability are the results of using conventional control tactics during grid failures. The advantages of SMC include its fast response time, insensitivity to uncertainty, and ability to handle nonlinearities. When it comes to faulttolerant control of DFIG, the two most common SMC approaches are: Using a Super-Twisting Algorithm for SMC Reduces buzzing and makes voltage more consistent. Control of Higher-Order Sliding Modes Manages electromagnetic torque, dampens torque waves, and offers reliable voltage and current management.

3.3 Super-Twisting Algorithm

The chattering problem, which results in excessive control effort and mechanical way, is a solution feature of SMC. An STA, a Second-Order Sliding Mode, can solve this problem a enabling a smooth control action while preserving resilience and reducing chattering. First 2 shows ne Super Twisting Algorithm.



ou er-Twisting Algorithm

Consider the DFIG rotor current control onder a voltage dip. The rotor current dynamics in the dq reference frame are given Eq. ().

$$\frac{di_r}{dt} = -\frac{R_r}{L_r}i_r + \frac{1}{L_r}(\nu_r - j\omega_s\psi_r)$$
(4)

Where, $i_r + p_d + p_r$ rotor currents in the dq reference frame, R_r, L_r means rotor resistance and inductive, $v_r + v_{rd} + p_{rq}$ rotor voltage, ω_s refers to synchronous speed, ψ_r means rotor flux. To regulate the rotor errent, define the sliding surface as:

$$S = i_r - i_r^* \tag{5}$$

 $1 \text{ i.e.} (5)_r^*$ is the reference rotor current. The control objective is to drive S to zero, ensuring accurate urrent tracking. The STA-SMC control input is designed as Eq. (6)

$$v_r = -k_1 |S|^{1/2} sign(S) - k_2 \int sign(S) dt$$
(6)

Where, k_1 , k_2 means positive control gain that can guarantee fast convergence, and sign(S) is the sign function that acts to implement the sliding mode. The benefits of STA-SMC for DFIG are that it reduces chattering, ensuring smooth control action. Enhances voltage stability by stabilizing the rotor current under grid faults. Faster response compared to conventional SMC.

3.4 Higher-Order Sliding Mode Control

The HOSMC algorithm controls electromagnetic torque during grid failures. HOSMC reduces torque ripple and overall harmonic distortion and ensures strong current and voltage control. Standard SMC control uses derivatives of the sliding variable to define and regulate action, whereas HOSMC uses higher-order derivatives, which may be smoother and overcome the high-frequency switching effect. DFIG-based wind turbines employ HOSMC for rotor current management to stabilize electromagnetic torque and produce electricity smoothly during grid voltage dips. The sliding surface is defined in Eq. (7).

$$S(x) = \lambda_0 x + \lambda_1 \dot{x} + \lambda_2 \ddot{x}$$

Where, λ_0 , λ_1 , λ_2 are positive control gains and *x* represents the system state variable (e.g., roto electromagnetic torque). The HOSMC control law is:

$$u = -k_1 |S|^{\frac{n}{m}} sign(S) - k_2 \int sign(S) dt$$

In Eq. (8) k_1, k_2 are control parameters. $\frac{n}{m}$ determines the sliding mode dvantages of HOSMC for DFIG are that it keeps the electromagnetic torque stable g ing vol ge dip. It reduces electromagnetic disturbances, enhancing power quality. Effectively ma DFIG rotor currents gip ensures grid stability. Combined Control Framework for the Integrated MPC TA + HOSMC Control integrates Model Predictive Control for wind turbine aerodynamics w ing Mode Control (incorporating Super-Twisting Algorithm and Higher Order SM IG stabilization under grid for (VSVP wind turbines get extracted power fault tolerance, and power disturbances. ficie production stability from these methods. MPC adjusts win pitc angle and generator torque in real time to maximize power coefficient. Real-time optic ation s future system states, allowing th pitch and torque changes. The DFIG control inputs to adapt quickly to energy hary d sñ ing control system receives the optimal torque point

Algorithm 1: VSVP Wind Turbine with DFIG
INPUT:
Wind speed (<i>Vw</i>), Blade pitch angle ($\underline{\beta}$), Rotor speed ∇_m)
Electrical torque (T_e) , Mechanical to que (T_m)
Stator and rotor currents (i_s, i_r)
Grid voltage (Vg), Converter V_{RSC} (V_{RSC} V_{GSC})
Reference active and reactive ower (Pt-67)
OUTPUT:
Optimized Blade Piter Ang. (β_{op})
Controlled Rotor V tage (V_{RS} control)
Fault Mitigation Response $(F_{r,ponse})$
Grid Kever geo n (1)
Step 1: Aet anamic antrol using MPC-Based Pitch Control
WE WE THE DO
No ure W. Speed
Computer Optimal Beta Angle using MPC
A first E. C. Pitch Angle (β)
Step 2. FIG Control using STA-SMC & HOSMC
Mea ure Rotor Speed (ω_m), Electromagnetic Torque (T_e)
Totor Speed > Rated Speed THEN
Apply STA-SMC Control
ELSE
Apply HOSMC Control
ENDIF
Step 3: Fault Detection and Mitigation
Fault Status ← Monitor System Anomalies
IF Fault Status == 1 THEN
SWITCH Control Mode
CASE "MPC":

Switch to STA-SMC for robustness CASE "STA-SMC": Switch to HOSMC for extreme fault cases ENDSWITCH Perform Fault Mitigation Strategy ENDIF Step 4: Power Conversion and Grid Integration Compute Rotor-Side Converter Control Compute Grid-Side Converter Control Regulate Active Power (*P*) and Reactive Power (*Q*) Step 5: Data Logging & System Monitoring Log Wind Speed, Rotor Speed, *P*, *Q*, Fault Status ENDWHILE END

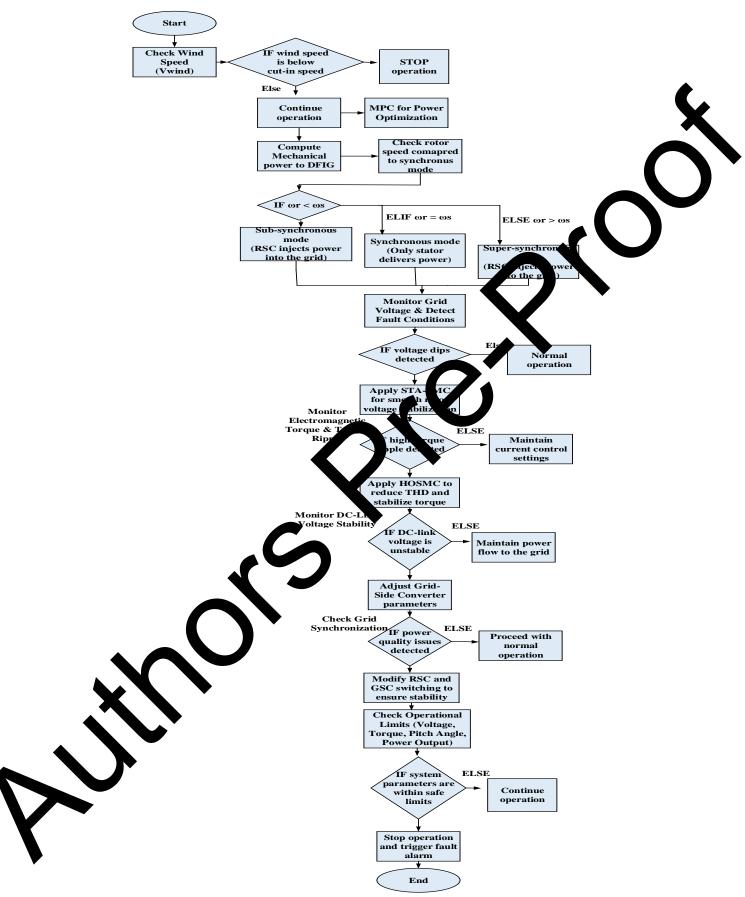


Fig. 3. Flow Chart

STA-SMC reduces chatter and smoothes control on the DFIG side to stabilize voltage during grid disruptions. Figure 3 shows how HOSMC controls electromagnetic torque with minimal torque ripple, Total Harmonic Distortion between currents, and strong voltage regulation. Therefore, STA and HOSMC enhance DFIG's FRT capacity, making the system exceptionally resilient against grid outages. The wind turbine and DFIG controls may share data. This allows an ideal torque set point input from the wind turbine to DFIG, which dynamically adjusts the generator's torque output in real time. This synchronized reaction of wind speed changes and grid disruption improves fault tolerance and power quality, making wind power production more efficient and steady.

4. Result and Discussion

The findings reveal DFIG-type wind turbine control system performance study. Variations in the and rotor voltage, current, torque, active and reactive power, and Fault Ride-Through behavior occompared to alternatives, power quality, torque ripple, and grid fault resilience increased

Establish aerodynamically reasonable power (λ) and limit wind turbing functioning, including rated power and wind speed. DFIG system parameters Jude v sistances, tages 16 GB RAM, and inductances, and frequencies. A powerful device with an Intel Core CP MATLAB/Simulink for modeling and analysis runs simulations. For istic control solution assessment, this environment simulates operations. The simulation para are: Wind turbine net $0^{\circ} - 25^{\circ}$, Tip Speed Ratio parameters: Rated power: 2MW, Rated wind speed: 0-25m/s, Pitch ang (λ):6 – 8, Pitch Angle Range:0° – 25°. DFIG Parameters: Rat 2MW, Stator Voltage:690 V (line-to-line), Rotor Voltage (via converter): 300 500 uency: 50 Hz.

4.1 Aerodynamic Performance of VSVP Wind Turk

The aerodynamic performance of a variable-seed variable sitch wind turbine is crucial for capturing more energy. The concept of power coefficient in vand energy conversion and its relationship to tip speed ratio. Pitch angle and generator torque have be precisely controlled for appropriate C_p . As wind conditions change, Model Predictive Control adjuts parameters to maximize power output without mechanical stress and optimize turbine performance during wind speed fluctuations.

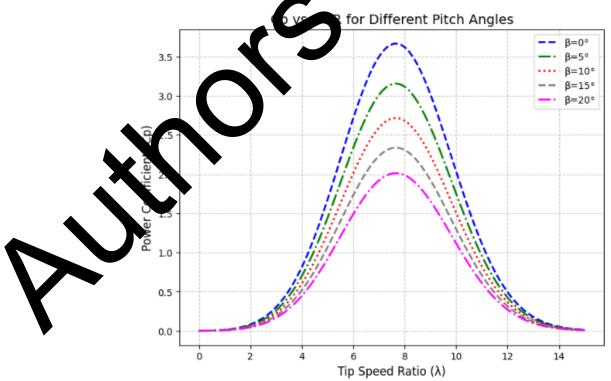


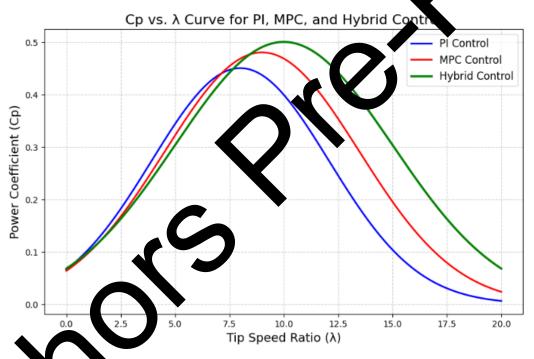
Fig. 4. Power Coefficient Vs Tip Speed Ratio

Figure 4 shows the power coefficient versus the λ at varying pitch angles (β). The trend indicates that C_p first rises with respect to TSR, reaches a maximum, and subsequently drops. Increasing the pitch angle decreases the peak C_p values and tends to draw the optimal TSR below. The efficiency study shows how pitch angle can influence turbine performance.

Tip Speed Ratio (λ)	PI Control (C_p)	MPC	Proposed Hybrid
4.5	0.38	0.42	0.46
5.5	0.40	0.46	0.50
6.5	0.42	0.48	0.52

Table 1: Power Coefficient vs. Tip Speed Ratio for Different Control Strategies

Table 1 shows the comparison of the power coefficient (C_p) , which illustrates the changes conducted by different control strategies, including PI control, MPC, and the proposed hybrid me nod an ifferent λ . The results show that this hybrid method obtains the greater C_p over all λ values, and furthermore, this method enables enhanced aerodynamic efficiency and better power extraction than the litional PI and MPC approaches.



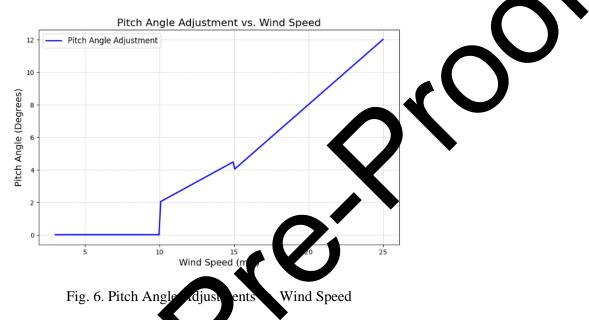
5. Power Coefficient vs. Tip Speed Ratio for Different Control Strategies

Figure 5 shows the C_p vs tip speed ratio for the PI, MPC, and Hybrid control strategies. It shows the performance chach of these control methods in extracting maximum power from the wind turbine. Is the Hybrid control has the highest peak C_p , this indicates greater efficiency at the TSR at which C_p is taxin zed. This leads to a slightly lower C_p peak value for the MPC control, but a wider range of peration with respect to power coefficient at higher TSRs. It suggests that a lower peak of power coefficient is captured by turbulent flow control and a reduced range are not able to collect power at different TSRs (often leading to a turbid flow).

4.1.1 Pitch Angle Optimization

Pitch angle control affects VSVP wind turbine aerodynamic performance. This is related to how pitch angles accept wind velocities to enhance power extraction and minimize overloading. Real-time pitch angle optimization improves smooth operation, mechanical stress, and fault tolerance. Figure 6 depicts

dynamic pitch angle changes under different wind conditions, proving that the control technique stabilized and optimized turbine performance. Figure 6 shows how wind speed affects wind turbine pitch angle adjustment. Under 10 m/s wind, the pitch angle is 0 degrees, as seen in the graph. The pitch angle increases exponentially with wind speed above this figure, reaching 2 degrees at 10 m/s and almost 12 degrees at 25 m/s. A tiny discontinuity at 15 m/s indicates a control strategy or turbine dynamics adjustment. This variant helps manage rotor speed and maximize power collection in varying wind conditions.



4.2 Performance Analysis of DFIG under Normal argufault Conditions

Studying the power flow, voltage, current, and to use characteristics of DFIG in the grid is necessary because to its varied functioning under different grid situations. The power interaction between the stator, rotor, and grid is examined at all operating modes: sub-synchronous, synchronous, and super-synchronous. This research also use an essentiate response to grid disturbances, including voltage, current, torque, active and refer we power fluctuations, and DC-link voltage stability. The charts above illustrate key parameters for uncerstanding system performance, normal and fault circumstances, and FRT capabilities.

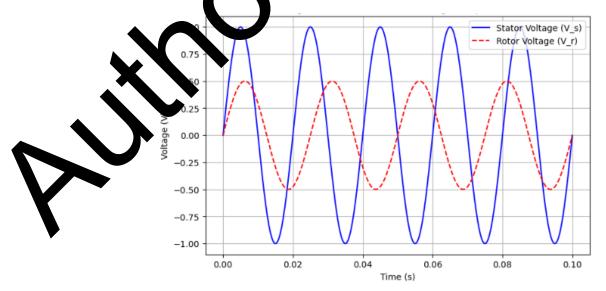
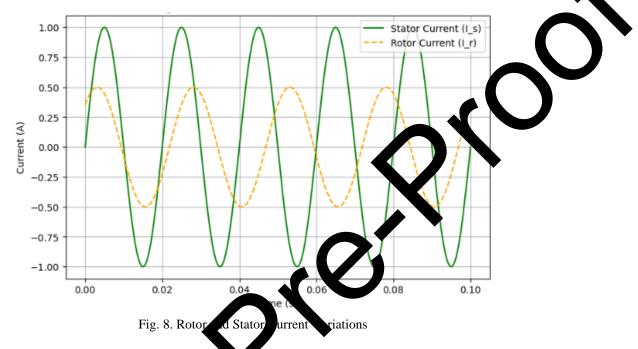


Fig.7. Stator and Rotor Voltage Response

The stator (*Vs*) and rotor (*Vr*) voltage response across 0.1 seconds is illustrated in Figure 7. This diagram indicates that both voltages propensity sinusoidally, but at separate amplitudes or phase factors. It can be seen that there is a higher amplitude on the stator voltage ranging from -1V to + 1V, and a lower amplitude on the rotor voltage, which varies from -0 - 5V to + 0 - 5V, and a phase shift between the rotor voltage and stator voltage. This operation is expected for induction machines and is representative of the induced voltage in the rotor with respect to the stator's magnetic field.



The stator (*Is*) and rotor (*Ir*) current changes over (0.1 sec) are illustrated in Figure 8. The generated sine currents are shown and the oscillation is sinusoidal as we for both currents, the green line representing the current of the stator where the current oscillating from (-1A, +A). The orange dashed line defines the rotor current from (-0.5A, +0.5A), which present 1 wer oscillating value and the rotor current with respect to stator current giving a phase difference lagging. This local as the rotor's induced current by the stator's magnetic field, one of the defining aspects of induction machines.

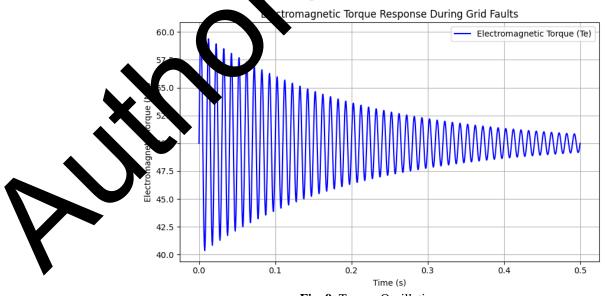


Fig. 9. Torque Oscillations

As shown in Figure 9, the electromagnetic torque Te response of the system during grid faults in the time period of 0–0.5 seconds. A torque graph with fault amplitude and time shows a drastic oscillation of time and then plateauing starting from the onset of the fault. The first peak is around 60 Nm and the troughs are roughly 40 Nm. These oscillations are a sign of transient instability through the grid fault. With time the oscillations decay, indicating that the system has the ability to rebound and settle. The exponential decay of the amplitude depends on the damping property of the system and its shock response.

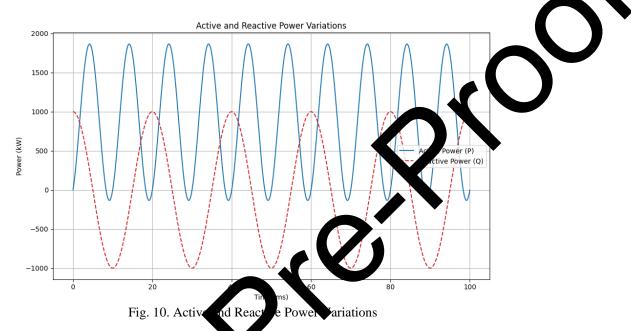


Figure 10 shows active power (P) and reactive power (Q) response in 100 ms. As seen from the graph, the curves of active and reactive power also scillate sinusoidally. The active power reaches a maximum value of about 2000 kW and a minimum of about 0 kW, the reactive power a maximum of 1000 kW and a minimum of -100 kW the power curves have a phase difference, which indicates an exchange of reactive power between the system and grid. These oscillation phenomena indicate the dynamic properties of the system with the variations of load or grid.

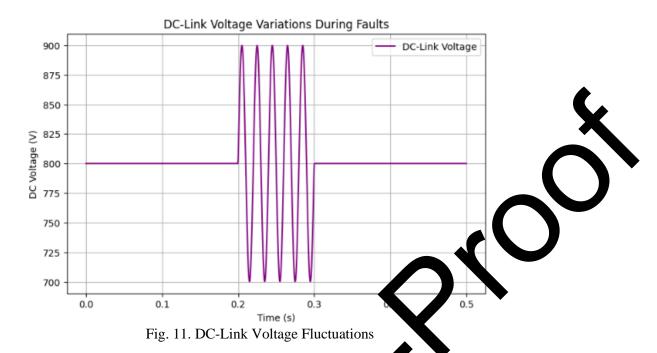
4.3 Fault-Tolerant Control ing Sta-SMC & HOSMC

onic Distortion are the biggest threats to DFIG-based wind energy Torque ripple and T al Hari systems. The suggest STA-SMC & HOSMC control framework reduces torque ripple and Hybr THD, de its importance in power quality. This enhances dynamic responsiveness over atih aranteeing smooth torque transmission and grid compliance. SMC, Super traditi rollers. m, and HOSMC significantly decrease chattering faults and enhance fault tolerance, Twisti lgon stable conditions regardless of grid disturbances and dynamic operating circumstances. guar teei

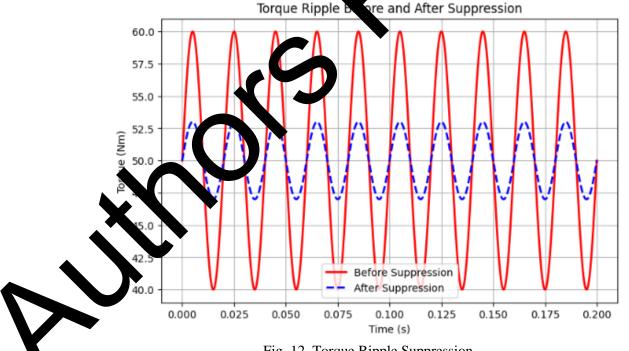
Table 2: Torque Ripple and THD Performance
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Parameter	Proposed Method (STA-SMC & HOSMC)
Torque Ripple (%)	1.8%
THD (%)	2.5%

This Table 2 entails the quantitative evaluation with respect to the proposed STA-SMC & the HOSMC method capable to bring an improvement up to a reduction of torque ripple and THD, making sure the direct torque delivery is enhanced under various grid conditions so that better power quality is ensured.



cond are indicated in Figure The variations of DC-link voltage in the presence of grid faults 11. The voltage would be there as a stable DC voltage +800V this up to about 0.2 seconds. ind s Then, from 0.2s to 0.3s, considerable oscillations exist, an es between 700V and 900V, age y and at 0.3s, the voltage returns to normal at 800V at the grid faults cause transient whic ndicat disturbance in DC-link voltage. Such a rapid yed by stabilization shows the response cilla ı fol and recovery of the system from fault cond on.





Torque ripple suppression for a period of 0.2 seconds is shown by Figure 12. Torque oscillations before suppression and after suppression (dashed blue line) are compared in the graph. The torque reads between 40 Nm and 60 Nm, which implies that the torque is quite fluctuating. After suppressing the oscillations, it varies between 47 Nm and 53 Nm, which is considered a significant improvement in its

performance regarding torque ripples and demonstrates improvement in stability and performance of the overall system. The suppress method works excellently in reducing torque variations; hence the operation becomes smooth.

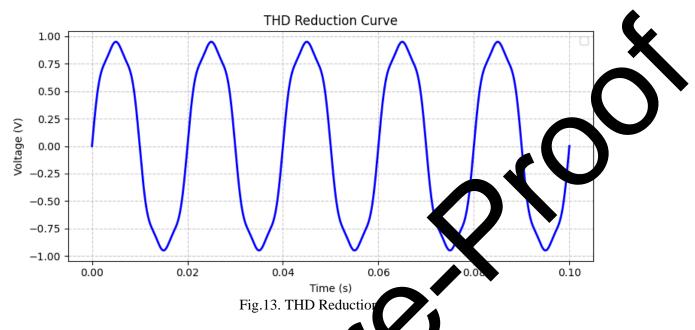


Figure 13 shows the reduction of Total Harmonic Distor on (1, **D**) for a period of 0.1 seconds. The report of the figure reflects a sinusoidal waveform to be writage, demonstrating a clear reduction in its harmonic content. The sine wave is smoothend very lose to what can be described as a perfect sine wave-the shadow of highly effective THD supression-and, therefore, shows better power quality. The constant amplitude and frequency throughout the period indicate the steady and effective THD reducing capability of the method.



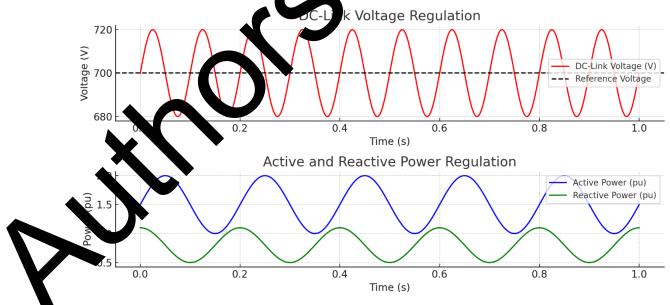


Fig. 14. DC-Link Voltage and Power Regulation

Wind energy conversion systems need solid grid integration to operate reliably. Regulation of DC-Link Voltage and Power DC-link voltage stability and active/reactive power regulation under various operating conditions are

shown in Figure 14. Low voltage fluctuations and fast stabilization are achieved using Hybrid MPC + STA + HOSMC management. According to the figure, the control framework improves DFIG-grid power exchange while preserving DC-link voltage. Transient overshoots, power oscillations, and grid instability are reduced via voltage management. Better dynamic responsiveness ensures strong Fault Ride-Through (FRT) and power quality using the recommended approach.

4.5 Performance Comparison

A comparison of the suggested Hybrid MPC + STA + HOSMC control system to PI, Fuzzy Logic, PID, and Sliding Mode Control is done to evaluate its efficacy. Performance criteria include fault ride-through (FR7, power quality (THD reduction), torque ripple minimization, and DC-link voltage stability. Grid integration, resistance to shocks, and steady-state performance improved significantly. The suggested method's performance is compared to existing methods in Table 3.

				_
Control Method	Fault Ride-Through	THD	To de	DC-Link Voltage
	Capability	Reduction (%)	R' de (%)	St. ility
PI Control Song et al.,[24]	Moderate	4.8		Moderate
Fuzzy Logic Aoun et al.,[27]	Moderate	4.2	5.9	Moderate
PID Control [29]	Moderate	4.0	5.5	Moderate
SMC [30]	High	3.5	4.8	High
Proposed (Hybrid MPC + STA + HOSMC)	Very High	X	2.3	Very High

Table 3: Performance Comparison	n with Existing Methods
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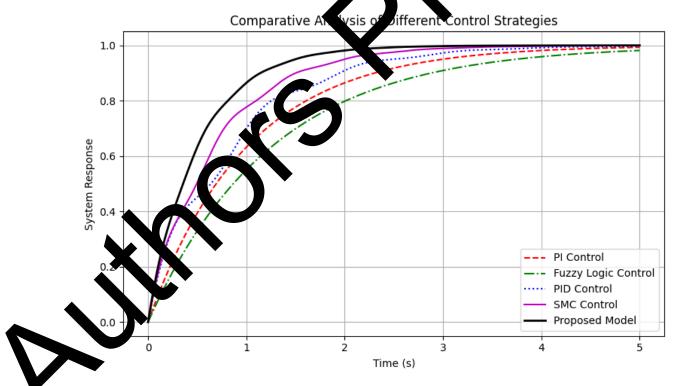


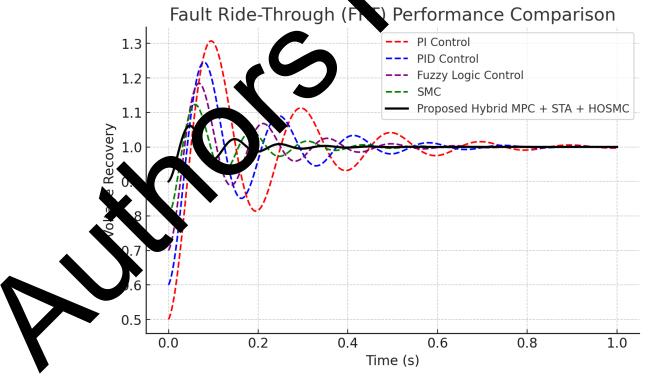
Fig.15. Comparative Analysis of Different Control Strategies

Figure 15 shows how different control strategies react within a period of 5 seconds. The "Proposed Model" has the fastest rise time and the fastest settling to a steady state of 1.0. In comparison, the performance of SMC and PID controls are very well but slower. Controllers PI and Fuzzy Logic react

slower and more settling time. It can be seen from the graph that the suggested model is fast and superior in stability over other control procedures.



The percentage of THD for PI, Fuzzy Logic, PID, SMC and Funose Hybrid control strategies are shown in this Figure 16. Among the proposed goal control, the input THD is the lowest, showing better power quality improvement. THD reduction is also much higher in SMC followed by PID and then Fuzzy Logic.



Fig, 17. Fault Ride-Through Performance

The Fault Ride-Through Performance Comparison Figure 17 demonstrates the performance of various control methods (including PI, PID, Fuzzy Logic, SMC and the proposed Hybrid MPC + STA +

HOSMC) during grid faults in the system. While conventional types takes a long time to recover and presents many oscillations, the proposed method effectively ensures quicker stabilization with negligible voltage and power oscillations. It emphasizes its better robustness than the provisioned under some faults in terms of maintaining the stable behavior of the power grid and reducing electromagnetic interference to the grid and being far more practical to use for DFIG-enabled wind turbines under realistic grid disturbances.

4.6 Discussion

A MPC, STA, and HOSMC control approach to improve DFIG wind turbine FRT, torque reduction and power quality. Different from PI, PID, Fuzzy Logic, and SMC, the suggested control approachieves greater aerodynamic efficiency, grid connection performance, and low Total Horomonic Distortion. MPC uses real-time pitch and torque control to maximize power from changing we situations, maximizing the Maximum Power Coefficient. STA-SMC reduces chattering and a rengthe grid resilience with HOSMC torque control refinement to minimize operation metabolic control approximation.

The suggested method offers fast fault detection, reduced magnetic inte rence and proved grid fault stability. Better grid compliance and power quality come from st dy DC nk voltage and less active and reactive power variability. Real-time optimization demands m rocessing power since hybrid control takes more calculation for precision. To optimize performance, ntroller settings must be fine-tuned under diverse operating situations. Future development show Include dynamic AI-based control parameter modifications and hardware-in-the-log ng for real-time validation. Implementing the method for multi-turbine wind farms with g capabilities will expand its rm application range for dependable big renewable power sys ems

5. Conclusion and Future Work

Under varying wind and grid conditions MPC STA + HOSMC control framework Hybri amplifies the performance along with stabil tog er with fault tolerance characteristics of DFIGbased wind turbines. The system produces maximum energy capture by reaching a power coefficient (Cp) of 0.52 when operating at its optimal tip spec ratio ($\lambda = 6.5$) thus surpassing both conventional \bigcirc gic controllers (Cp = 0.48). The FRT functionality receives PI controllers (Cp = 0.42) and Fuzz expanded capability which enables atisf grid code requirements through sustaining an optimal DClink voltage range at low-volt ge condition disturbances. Better power quality results from a Total el of 1.5.7 while performance surpasses the levels of 3.5% (PI), 2.8% Harmonic Distortion (THD) col). The proposed approach produces torque ripple at 2.1% which (PID) and 2.3% (Fuzzy co exceeds both 4.5% () and . (SMC) by providing lower levels and leads to smoother turbine operation with reduce necha cal stress. A main challenge for the proposed framework exists in its computat xitymen applying it to real-time control because hardware components need COM er. The setup of parameters in controllers needs adaptive modifications during increa ssing p al settings to achieve maximum system performance. differe perat

The neure evelopment will emphasize AI-based adaptive optimization to make real-time adjustments of control parameters according to fluctuating wind conditions and grid situations. The implementation wough hadware-in-the-loop methods and real-time testing will confirm operational feasibility. The approach when implemented to multi-turbine wind farms that can function as grid formers will improve integration of big renewable energy projects. Predictive maintenance which integrates AI and IoT technology enables operators to enhance operational reliability of their systems. The stability and resilience of renewable energy systems will be improved through the study of hybrid energy systems which use storage solutions of batteries or hydrogen systems.

Conflicts of interest: The authors have no conflicts of interest to declare.

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